# Static Output Feedback Control for Discrete-time **Piecewise Linear Systems: an LMI Approach**

DING Da-Wei<sup>1, 2</sup> YANG Guang-Hong<sup>1, 2</sup>

Abstract This paper investigates the problem of static output feedback (SOF) control for discrete-time piecewise linear systems. Based on piecewise quadratic Lyapunov functions, new sufficient LMI conditions for the synthesis of SOF stabilization controllers are presented. Meanwhile, by using Finsler's lemma, a set of slack variables with special structure are introduced to reduce design conservatism. Compared to the existing methods, the proposed method has a good performance and can work successfully in situations where the existing methods fail. An extension of this method is also given in order to incorporate  $H_{\infty}$  performance. Three examples are given to illustrate the effectiveness of our method.

Key words Piecewise linear systems, piecewise quadratic Lyapunov function, Finsler's lemma, static output feedback (SOF), linear matrix inequality (LMI)

Piecewise linear systems have been receiving much attention in control and system and circuit communities because a large class of nonlinear systems, such as systems with relay, saturation, or dead-zone, can be modeled as piecewise linear systems<sup>[1]</sup>. In fact, piecewise linear systems are a broad modeling class in the sense that they have been shown to be equivalent to many other classes of systems, such as mixed logic dynamical systems<sup>[2]</sup> and extended linear complementary systems<sup>[3]</sup>.

Since [4] presented a pioneering work on the analysis of discrete-time piecewise linear systems in the early 1980 s, numerous results<sup>[1-17]</sup> have been obtained on analysis and synthesis of piecewise linear systems. For example, [6-7] presented results on stability and optimal performance analysis for continuous-time piecewise linear systems based on a piecewise quadratic Lyapunov function. Reference [16] extended the stability analysis method of [6] to discrete-time piecewise linear systems. Meanwhile, controller design for piecewise linear systems arose, such as [8-11] for continuous-time systems and [15, 17] for discretetime systems. For stability analysis and control synthesis of piecewise linear systems, there are two major differences between the continuous-time and discrete-time  $case^{[12]}$ . First, in the former, only continuous Lyapunov functions can be used, whereas in the latter, discontinuous Lyapunov functions are also allowed. Second, in the discrete-time case, switching can also occur between non-adjacent regions and this fact must be properly handled in analysis and synthesis algorithms.

On the other hand, static output feedback (SOF) is one of the most important open problems in control theory and practice. It represents the simplest closed-loop control system, which can be easily implemented with low cost. Therefore, the problem has been extensively studied for the past decades. To deal with the SOF control problem of linear systems, there are various approaches; see [18-21] and references therein.

This paper studies the problem of SOF control for discrete-time piecewise linear systems. In [22-23], the

DOI: 10.3724/SP.J.1004.2009.00337

problem of SOF control for discrete-time switched linear systems was investigated and sufficient LMI conditions were given to obtain controller gains. These two methods are also applicable to discrete-time piecewise linear systems. In this paper, based on piecewise quadratic Lyapunov functions, new sufficient LMI conditions for the synthesis of SOF stabilization controllers are given. Meanwhile, by using Finsler's lemma, a set of slack variables with special structure are introduced to reduce design conservatism. Compared to the methods in [22-23], our method proves to have a good performance and can work successfully in situations where the methods in [22-23] do not. In addition, an extension of this method is also given in order to incorporate  $H_{\infty}$  performance.

The rest of the paper is organized as follows. Section 1 gives the problem statement. Section 2 gives new sufficient LMI-based conditions for SOF stabilization of discrete-time piecewise linear systems. Section 3 extends the method to  $H_{\infty}$  SOF control. Section 4 gives three examples to illustrate the effectiveness of the proposed methods. Finally, we conclude the paper in Section 5.

Notations. We use standard notations throughout this paper.  $M^{\mathrm{T}}$  is the transpose of matrix M and  $M^{-\mathrm{T}}$  means  $(M^{-1})^{\mathrm{T}}$ . M > 0 (< 0) means that M is positive (negative) definite. The symbol "\*" is used in some matrix expressions to induce a symmetric structure.  $L^2$  is the Lebesgue space consisting of all discrete-time vector-valued functions that are square-summable over  $[0, 1, 2, \cdots, \infty)$ .

#### 1 **Problem statement**

Consider the following discrete-time piecewise linear system

$$\begin{cases} \boldsymbol{x}(k+1) = A_i \boldsymbol{x}(k) + B_i \boldsymbol{u}(k) \\ \boldsymbol{y}(k) = C_i \boldsymbol{x}(k) \end{cases}, \text{ for } \boldsymbol{x} \in X_i, i \in I_l \quad (1)$$

where  $\boldsymbol{x}(k) \in \mathbf{R}^n$  is the state,  $\boldsymbol{u}(k) \in \mathbf{R}^m$  is the control input, and  $\boldsymbol{y}(k) \in \mathbf{R}^p$  is the measured output.  $\{X_i\}_{i \in I_1} \subseteq$  $\mathbf{R}^n$  denotes a partition of the state space X into a number of closed polyhedral subspaces, i.e.,  $I_l = \{1, 2, \dots, l\}$  is the index set of subspaces. We refer to each  $X_i$  as a cell. Let S be the set of all ordered pairs (i, j) of indices, denoting the possible switches from cell i to cell j

$$S = \{(i,j): i, j \in I_l \text{ such that } \boldsymbol{x}(k) \in X_i \text{ and } \boldsymbol{x}(k+1) \in X_j\}$$
(2)

The set S can be determined via reachability analysis for mixed logic dynamical (MLD) systems<sup>[2]</sup>.

In this paper, we investigate the SOF stabilization problem, i.e., the problem of designing a static output feedback

Received January 7, 2008; in revised form August 14, 2008 Supported by the State Key Program of National Natural Science of China (60534010), National Basic Research Program of China (973 Program) (2009CB320604), National Natural Science Founda-tion of China (60674021), the Funds for Creative Research Groups of China (60521003), the 111 Project (B08015), and the Funds of Ph. D. Program of Ministry of Eduction, China (20060145019) 1. Key Laboratory of Integrated Automation of Process Industry, Ministry of Education, Northeastern University, Shenyang 110004, P.R. China 2. College of Information Science and Engineering, Northeastern University, Shenyang 110004, P. R. China DOI: 10.3724/SP.L1004.2009.00337

control law

$$\boldsymbol{u}(k) = K_i \boldsymbol{y}(k), \quad i \in I_l \tag{3}$$

such that the closed-loop piecewise linear system

$$\boldsymbol{x}(k+1) = A_{cli}\boldsymbol{x}(k) \tag{4}$$

$$A_{cli} = A_i + B_i K_i C_i \tag{5}$$

is exponentially stable.

Without loss of generality, it is assumed that  $B_i$  (or  $C_i$ ),  $i = 1, 2, \dots, l$  are of full column (or row) rank. Then, there exist nonsingular transformation matrices  $T_{bi}$  (or  $T_{ci}$ ), i = $1, 2, \cdots, l$  such that

$$T_{bi}B_i = \left[\begin{array}{c}I\\0\end{array}\right] \tag{6}$$

$$C_i T_{ci} = \begin{bmatrix} I & 0 \end{bmatrix} \tag{7}$$

Note that for any given  $B_i$  (or  $C_i$ ), the corresponding  $T_{bi}$ (or  $T_{ci}$ ) are generally not unique. Special  $T_{bi}$  and  $T_{ci}$  can be obtained by

$$T_{bi} = \begin{bmatrix} (B_i^{\mathrm{T}} B_i)^{-1} B_i^{\mathrm{T}} \\ B_i^{\mathrm{T} \perp \mathrm{T}} \end{bmatrix}$$
(8)

$$T_{ci} = \begin{bmatrix} C_i^{\mathrm{T}} (C_i C_i^{\mathrm{T}})^{-1} & C_i^{\perp} \end{bmatrix}$$
(9)

where  $B_i^{\mathrm{T} \perp \mathrm{T}}$  denotes the transpose of an orthogonal basis for the null space of  $B_i^{\mathrm{T}}$ , and  $C_i^{\perp}$  denotes an orthogonal basis for the null space of  $C_i$ .

The following lemmas are useful throughout this paper. Lemma 1 (Finsler's lemma). Let  $\boldsymbol{\xi} \in \mathbf{R}^n$ ,  $P = P^{\mathrm{T}} \in \mathbf{R}^{n \times n}$ , and  $H \in \mathbf{R}^{m \times n}$  such that  $\operatorname{rank}(H) = r < n$ ; then the following statements are equivalent:

1)  $\boldsymbol{\xi}^{\mathrm{T}} \mathcal{P} \boldsymbol{\xi} < 0$ , for all  $\boldsymbol{\xi} \neq 0$ ,  $\hat{H} \boldsymbol{\xi} = 0$ ;

2)  $\exists X \in \mathbf{R}^{n \times m}$  such that  $P + XH + H^{\mathrm{T}}X^{\mathrm{T}} < 0$ . Lemma  $\mathbf{2}^{[13, 15]}$ . If there exist matrices  $P_i = P_i^{\mathrm{T}} > 0$ ,  $\forall i \in I_l$  such that the positive definite function  $V(\boldsymbol{x}) =$  $\boldsymbol{x}^{\mathrm{T}} P_i \boldsymbol{x}, \forall \boldsymbol{x} \in X_i \text{ satisfies } V(\boldsymbol{x}(k+1)) - V(\boldsymbol{x}(k)) < 0, \text{ then}$ the closed-loop piecewise linear system (4) is exponentially stable.

The piecewise quadratic Lyapunov function appearing in Lemma 2 can be computed as<sup> $[\bar{1}3, 15]$ </sup>

$$\begin{aligned} A_{cli}^{\mathrm{T}} P_j A_{cli} - P_i < 0, \quad \forall (i,j) \in S \\ P_i = P_i^{\mathrm{T}} > 0, \quad \forall i \in I_l \end{aligned}$$

where S is given in (2).

#### 2 SOF stabilization

In this section, based on a piecewise quadratic Lyapunov function and Finsler's lemma, new sufficient LMI conditions are deduced to obtain the SOF control gains  $K_i$ .

**Theorem 1.** Assume that  $B_i$ ,  $i = 1, 2, \dots, l$  are of full column rank. If there exist symmetric matrices  $\bar{P}_i$ ,  $\bar{P}_j \in \mathbf{R}^{n \times n}$ , and matrices  $G_i \in \mathbf{R}^{n \times n}$ ,  $L_i \in \mathbf{R}^{n \times p}$  with the following structure

$$G_i = \begin{bmatrix} G_{i11} & G_{i12} \\ 0 & G_{i22} \end{bmatrix}, \quad L_i = \begin{bmatrix} L_{i1} \\ 0 \end{bmatrix}$$
(10)

satisfying the inequalities

$$\begin{bmatrix} \bar{P}_j - G_i - G_i^{\mathrm{T}} & G_i \bar{A}_i + L_i \bar{C}_i \\ * & -\bar{P}_i \end{bmatrix} < 0, \quad \forall (i,j) \in S \quad (11)$$

where

$$\bar{A}_i = T_{bi} A_i T_{bi}^{-1}, \quad \bar{C}_i = C_i T_{bi}^{-1}$$
 (12)

and  $T_{bi}$  are given by (8), then the closed-loop piecewise linear system (4) is exponentially stable and the control gain  $K_i$  can be obtained by

$$K_i = G_{i11}^{-1} L_{i1}, \quad i \in I_l \tag{13}$$

**Proof.** Assume that LMIs (11) are feasible. From the structure of  $L_i$  and  $G_i$ , and from (6) and (13), we can obtain

$$L_{i} = \begin{bmatrix} L_{i1} \\ 0 \end{bmatrix} = \begin{bmatrix} G_{i11}K_{i} \\ 0 \end{bmatrix} = \begin{bmatrix} G_{i11} & G_{i12} \\ 0 & G_{i22} \end{bmatrix} \begin{bmatrix} I \\ 0 \end{bmatrix} K_{i} = G_{i}T_{bi}B_{i}K_{i}$$
(14)

Define  $P_i = T_{bi}^{\mathrm{T}} \bar{P}_i T_{bi}, P_i = T_{bi}^{\mathrm{T}} \bar{P}_i T_{bi}$ , then

$$\bar{P}_j = T_{bi}^{-\mathrm{T}} P_j T_{bi}^{-1}, \quad \bar{P}_i = T_{bi}^{-\mathrm{T}} P_i T_{bi}^{-1} \tag{15}$$

Substituting (12), (14), and (15) into (11), we have

$$\begin{bmatrix} T_{bi}^{-T}P_{j}T_{bi}^{-1} - G_{i} - G_{i}^{T} & \Xi_{i} \\ * & -T_{bi}^{-T}P_{i}T_{bi}^{-1} \end{bmatrix} < 0, \\ \forall (i,j) \in S \qquad (16)$$

where  $\Xi_i = G_i T_{bi} A_i T_{bi}^{-1} + G_i T_{bi} B_i K_i C_i T_{bi}^{-1}$ . Pre- and post-multiplying (16) by  $\begin{bmatrix} T_{bi}^{\mathrm{T}} & 0\\ 0 & T_{bi}^{\mathrm{T}} \end{bmatrix}$  and its transpose, we have

$$\begin{bmatrix} P_j - T_{bi}^{\mathrm{T}} G_i T_{bi} - T_{bi}^{\mathrm{T}} G_i^{\mathrm{T}} T_{bi} & T_{bi}^{\mathrm{T}} G_i T_{bi} A_{cli} \\ * & -P_i \end{bmatrix} < 0,$$
$$\forall (i,j) \in S \quad (17)$$

Inequalities (17) can be written in the form

$$P + XH + H^{\mathrm{T}}X^{\mathrm{T}} < 0, \quad \forall (i,j) \in S$$
(18)

where

$$P = \begin{bmatrix} P_j & 0\\ 0 & -P_i \end{bmatrix}, \quad X = \begin{bmatrix} T_{bi}^{\mathrm{T}}G_iT_{bi}\\ 0 \end{bmatrix}$$
$$H = \begin{bmatrix} -I & A_{cli} \end{bmatrix}$$
(19)

Define  $\boldsymbol{\xi} = \begin{bmatrix} \boldsymbol{x}(k+1) \\ \boldsymbol{x}(k) \end{bmatrix}$ , then the closed-loop system (4) can be written in the form

$$H\boldsymbol{\xi} = 0 \tag{20}$$

It follows from Finsler's lemma that (18) is equivalent to

$$\boldsymbol{\xi}^{\mathrm{T}} P \boldsymbol{\xi} < 0, \quad \forall (i,j) \in S$$
(21)

Then, we have

$$\begin{bmatrix} \boldsymbol{x}^{\mathrm{T}}(k+1) & \boldsymbol{x}^{\mathrm{T}}(k) \end{bmatrix} \begin{bmatrix} P_{j} & 0\\ 0 & -P_{i} \end{bmatrix} \begin{bmatrix} \boldsymbol{x}(k+1)\\ \boldsymbol{x}(k) \end{bmatrix} < 0,$$
$$\forall (i,j) \in S \quad (22)$$

that is,

$$\boldsymbol{x}^{\mathrm{T}}(k+1)P_{j}\boldsymbol{x}(k+1) - \boldsymbol{x}^{\mathrm{T}}(k)P_{i}\boldsymbol{x}(k) < 0, \quad \forall (i,j) \in S \ (23)$$

with

Substituting (4) into (23) obtains

$$A_{cli}^{\mathrm{T}} P_j A_{cli} - P_i < 0, \quad \forall (i,j) \in S$$

It follows from (11) and (15) that

$$P_i = P_i^{\mathrm{T}} > 0, \quad \forall i \in I_i$$

Based on Lemma 2, the closed-loop piecewise linear system (4) is exponentially stable.

Note that the invertibility of  $G_{i11}$  can be assured by condition (11) in Theorem 1. See the following lemma.

**Lemma 3.** If LMIs (11) are feasible, then  $G_{i11}$  are invertible.

**Proof.** It follows from (11) that

$$\begin{split} \bar{P}_j - G_i - G_i^{\mathrm{T}} < 0, \quad \forall (i,j) \in S \\ - \bar{P}_i < 0, \quad \forall i \in I_l \end{split}$$

then, we have  $G_i + G_i^{\mathrm{T}} > \bar{P}_j > 0$ . This implies  $G_i$  are invertible<sup>[24]</sup>. Therefore,  $G_{i11}$ , the block (1, 1) of  $G_i$ , are invertible.  $\square$ 

In the same way, the invertibility of  $G_{i11}$  can be assured by the conditions of Theorems  $2 \sim 4$  below.

**Theorem 2.** Assume that  $C_i$ ,  $i \in I_l$  are of full row rank. If there exist symmetric matrices  $\bar{P}_i$  and  $\bar{P}_j \in \mathbf{R}^{n \times n}$ , and matrices  $G_i \in \mathbf{R}^{n \times n}$  and  $L_i \in \mathbf{R}^{m \times n}$  with the following structure

$$G_i = \begin{bmatrix} G_{i11} & 0 \\ G_{i21} & G_{i22} \end{bmatrix}, \quad L_i = \begin{bmatrix} L_{i1} & 0 \end{bmatrix}$$
(24)

satisfying the inequalities

$$\begin{bmatrix} \bar{P}_j - G_i - G_i^{\mathrm{T}} & * \\ \bar{A}_i G_i + \bar{B}_i L_i & -\bar{P}_i \end{bmatrix} < 0, \quad \forall (i,j) \in S$$
 (25)

where

$$\bar{A}_i = T_{ci}^{-1} A_i T_{ci}, \quad \bar{B}_i = T_{ci}^{-1} B_i$$
 (26)

and  $T_{ci}$  are given by (9), then the closed-loop piecewise linear system (4) is exponentially stable and the control gain  $K_i$  can be obtained by

$$K_i = L_{i1} G_{i11}^{-1}, \quad i \in I_l \tag{27}$$

**Proof.** From the structure of  $L_i$  and  $G_i$ , and from (7) and (27), we can obtain

$$L_{i} = \begin{bmatrix} L_{i1} & 0 \end{bmatrix} = \begin{bmatrix} K_{i}G_{i11} & 0 \end{bmatrix} =$$

$$K_{i} \begin{bmatrix} I & 0 \end{bmatrix} \begin{bmatrix} G_{i11} & 0 \\ G_{i21} & G_{i22} \end{bmatrix} = K_{i}C_{i}T_{ci}G_{i} \qquad (28)$$

Define  $P_i = T_{ci} \bar{P}_i T_{ci}^{\mathrm{T}}$ ,  $P_i = T_{ci} \bar{P}_i T_{ci}^{\mathrm{T}}$ , then

$$\bar{P}_j = T_{ci}^{-1} P_j T_{ci}^{-\mathrm{T}}, \quad \bar{P}_i = T_{ci}^{-1} P_i T_{ci}^{-\mathrm{T}}$$
 (29)

Substituting (26), (28), and (29) into (25), we have

$$\begin{bmatrix} T_{ci}^{-1}P_{j}T_{ci}^{-T} - G_{i} - G_{i}^{T} & * \\ T_{ci}^{-1}A_{i}T_{ci}G_{i} + T_{ci}^{-1}B_{i}K_{i}C_{i}T_{ci}G_{i} & -T_{ci}^{-1}P_{i}T_{ci}^{-T} \end{bmatrix} < 0, \\ \forall (i,j) \in S \ (30)$$

Pre- and post-multiplying (30) by  $\begin{bmatrix} T_{ci} & 0\\ 0 & T_{ci} \end{bmatrix}$  and its transpose, we have

$$\begin{bmatrix} P_j - T_{ci}G_iT_{ci}^{\mathrm{T}} - T_{ci}G_i^{\mathrm{T}}T_{ci}^{\mathrm{T}} & *\\ A_{cli}T_{ci}G_iT_{ci}^{\mathrm{T}} & -P_i \end{bmatrix} < 0, \quad \forall (i,j) \in \mathcal{S}$$

$$\tag{31}$$

Inequalities (31) can be rewritten in the following form

$$P + XH + H^{\mathrm{T}}X^{\mathrm{T}} < 0, \quad \forall (i,j) \in S$$
(32)

where

$$P = \begin{bmatrix} P_j & 0\\ 0 & -P_i \end{bmatrix}, \quad X = \begin{bmatrix} T_{ci}G_iT_{ci}^{\mathrm{T}}\\ 0 \end{bmatrix}, \quad H = \begin{bmatrix} -I & A_{cli}^{\mathrm{T}} \end{bmatrix}$$

Consider the dual system of (4)

$$\boldsymbol{x}'(k+1) = A_{cli}^{\mathrm{T}} \boldsymbol{x}'(k) \tag{33}$$

Define  $\boldsymbol{\xi}' = \begin{bmatrix} \boldsymbol{x}'(k+1) \\ \boldsymbol{x}'(k) \end{bmatrix}$ . Then, (33) can be rewritten in the form  $H\mathbf{\xi}' = 0$ 

From Finsler's lemma, we know that (32) is equivalent to

$$\boldsymbol{\xi}^{\prime \mathrm{T}} P \boldsymbol{\xi}^{\prime} < 0 \tag{35}$$

then, we have

$$\begin{bmatrix} \boldsymbol{x}'^{\mathrm{T}}(k+1) & \boldsymbol{x}'^{\mathrm{T}}(k) \end{bmatrix} \begin{bmatrix} P_{j} & 0\\ 0 & -P_{i} \end{bmatrix} \begin{bmatrix} \boldsymbol{x}'(k+1)\\ \boldsymbol{x}'(k) \end{bmatrix} < 0,$$
$$\forall (i,j) \in S$$
(36)

that is,

$$\boldsymbol{x}^{'^{\mathrm{T}}}(k+1)P_{j}\boldsymbol{x}^{'}(k+1) - \boldsymbol{x}^{'^{\mathrm{T}}}(k)P_{i}\boldsymbol{x}^{'}(k) < 0, \quad \forall (i,j) \in S$$
(37)

Substituting (33) into (37) yields

$$(A_{cli}^{\mathrm{T}})^{\mathrm{T}} P_j A_{cli}^{\mathrm{T}} - P_i < 0, \quad \forall (i,j) \in S$$

It follows from (25) and (29) that

$$P_i = P_i^{\mathrm{T}} > 0, \quad \forall i \in I_l$$

Based on Lemma 2, the closed-loop piecewise linear system (4) is exponentially stable.

Remark 1. Theorems 1 and 2 present new sufficient LMI-based conditions for SOF stabilization control for discrete-time piecewise linear systems. These conditions are convex and numerically well tractable with commer-cially available software<sup>[25-26]</sup>. Free slack variables  $G_i$  with special structure are introduced to reduce design conservatism.

Remark 2. For discrete-time piecewise linear systems, the state may switch among non-adjacent regions of the state-space partition. In this paper, we define the set S that contains all the ordered pairs of indices denoting the possible switches and can be computed via reachability analysis for MLD systems<sup>[2]</sup>. However, when designing an SOF controller, the set of all possible switches is seldom known in advance, and it may be necessary to consider all pairs of indices in  $S_{all} = I_l \times I_l$ . Therefore, our synthesis approach in Theorems 1 and 2 can be used to design SOF control for discrete-time switched linear systems with arbitrary switching.

Remark 3. The proposed method is different from that in [22], where equality constraint was imposed on Lyapunov matrics  $P_i$  or slack variables  $G_i$ . It also differs from the method in [23], which works well only when matrix  $A_i^{(22)}$ (the block (2,2) of  $A_i$ ) are Schur stable. Numerical examples (in Section 4) will show that our method can work successfully in situations where [22-23] do not.

## 3 Extension to $H_{\infty}$ SOF control

Consider the following discrete-time piecewise linear system

$$\begin{cases} \boldsymbol{x}(k+1) = A_i \boldsymbol{x}(k) + B_{i1} \boldsymbol{u}(k) + B_{i2} \boldsymbol{w}(k) \\ \boldsymbol{z}(k) = C_{i1} \boldsymbol{x}(k) + D_{i11} \boldsymbol{u}(k) + D_{i12} \boldsymbol{w}(k) \\ \boldsymbol{y}(k) = C_{i2} \boldsymbol{x}(k) + D_{i21} \boldsymbol{w}(k) \end{cases}$$
(38)

for  $\boldsymbol{x}(k) \in X_i$ ,  $i \in I_i$ , where  $\boldsymbol{x}(k) \in \mathbf{R}^n$  is the system state,  $\boldsymbol{u}(k) \in \mathbf{R}^m$  is the control input,  $\boldsymbol{w}(k) \in \mathbf{R}^r$  is disturbance input,  $\boldsymbol{z}(k) \in \mathbf{R}^q$  is the controlled output, and  $\boldsymbol{y}(k) \in \mathbf{R}^p$  is the measured output. Let S be the set of all ordered pairs (i, j) of indices, denoting the possible switches from cell ito cell j

$$S = \{(i, j) : i, j \in I_l \text{ such that } \boldsymbol{x}(k) \in X_i \text{ and } \boldsymbol{x}(k+1) \in X_j\}$$
(39)

In this section, we will design SOF control for the discrete-time piecewise linear system (38) in the  $H_{\infty}$  framework: Given a real number  $\gamma > 0$ , the exogenous signal  $\boldsymbol{w}$  is attenuated by  $\gamma$  if, assuming  $\boldsymbol{x}(0) = \boldsymbol{0}$ , for each integer  $N \geq 0$  and for every  $\boldsymbol{w} \in L_2([0, N], \mathbf{R}^r)$ 

$$\sum_{k=0}^{N} \|\boldsymbol{z}(k)\|^2 < \gamma^2 \sum_{k=0}^{N} \|\boldsymbol{w}(k)\|^2$$
(40)

With the controller (3), the closed-loop piecewise linear system becomes

$$\begin{cases} \boldsymbol{x}(k+1) = A_{cli}\boldsymbol{x}(k) + B_{cli}\boldsymbol{w}(k) \\ \boldsymbol{z}(k) = C_{cli}\boldsymbol{x}(k) + D_{cli}\boldsymbol{w}(k) \end{cases}, \text{ for } i \in I_l \quad (41)$$

where

$$A_{cli} = A_i + B_{i1}K_iC_{i2}, \qquad B_{cli} = B_{i2} + B_{i1}K_iD_{i21}$$
$$C_{cli} = C_{i1} + D_{i11}K_iC_{i2}, \qquad D_{cli} = D_{i12} + D_{i11}K_iD_{i21}(42)$$

Without loss of generality, we assume that  $B_{i1}$  (or  $C_{i2}$ ),  $i = 1, \dots, l$  are of full column (or row) rank. Then, there exist nonsingular transformation matrices  $T_{bi}$  (or  $T_{ci}$ ),  $i = 1, \dots, l$  such that

$$T_{bi}B_{i1} = \begin{bmatrix} I \\ 0 \end{bmatrix}, \quad C_{i2}T_{ci} = \begin{bmatrix} I & 0 \end{bmatrix}$$
(43)

Note that for any given  $B_{i1}$  (or  $C_{i2}$ ), the corresponding  $T_{bi}$  (or  $T_{ci}$ ) are generally not unique. Special  $T_{bi}$  and  $T_{ci}$  can be given as

$$T_{bi} = \begin{bmatrix} (B_{i1}^{\mathrm{T}} B_{i1})^{-1} B_{i1}^{\mathrm{T}} \\ B_{i1}^{\mathrm{T} \perp \mathrm{T}} \end{bmatrix}, \quad T_{ci} = \begin{bmatrix} C_{i2}^{\mathrm{T}} (C_{i2} C_{i2}^{\mathrm{T}})^{-1} & C_{i2}^{\perp} \end{bmatrix}$$
(44)

The following lemma is useful in this section.

**Lemma 4**<sup>[13, 15]</sup>. Consider the piecewise linear system (38) with zero initial condition  $\boldsymbol{x}(0) = \boldsymbol{0}$ . If there exists a function  $V(\boldsymbol{x}) = \boldsymbol{x}^{\mathrm{T}} P_i \boldsymbol{x}, \forall \boldsymbol{x} \in X_i$  with  $P_i = P_i^{\mathrm{T}} > 0$  satisfying the following inequality

$$V(\boldsymbol{x}(k+1)) - V(\boldsymbol{x}(k)) < \gamma^2 \|\boldsymbol{w}(k)\|^2 - \|\boldsymbol{z}(k)\|^2, \quad \forall k$$
 (45)

then the  $H_{\infty}$  performance condition (40) is satisfied. Furthermore, the closed-loop piecewise linear system (41) is exponentially stable.

The piecewise quadratic Lyapunov function appearing in Lemma 3 can be computed  $\mathrm{as}^{[13,\ 15]}$ 

$$\begin{split} \boldsymbol{x}^{\mathrm{T}}(k+1)P_{j}\boldsymbol{x}(k+1) - \boldsymbol{x}^{\mathrm{T}}(k)P_{i}\boldsymbol{x}(k) < \\ \gamma^{2}\boldsymbol{w}^{\mathrm{T}}(k)\boldsymbol{w}(k) - \boldsymbol{z}^{\mathrm{T}}(k)\boldsymbol{z}(k), \quad \forall (i,j) \in S \end{split}$$

and

$$P_i = P_i^T > 0, \quad \forall i \in I_i$$

Now, we give sufficient LMI conditions to obtain  $H_{\infty}$  SOF control gains  $K_i$ .

**Theorem 3.** Assume that  $D_{i11}$  are null matrices and  $B_{i1}$ ,  $i = 1, \dots, l$  are full column rank matrices. If there exist symmetric matrices  $\bar{P}_i$  and  $\bar{P}_j \in \mathbf{R}^{n \times n}$  and matrices  $G_i \in \mathbf{R}^{n \times n}$  and  $L_i \in \mathbf{R}^{n \times p}$  with the following structure

$$G_i = \begin{bmatrix} G_{i11} & G_{i12} \\ 0 & G_{i22} \end{bmatrix}, \quad L_i = \begin{bmatrix} L_{i1} \\ 0 \end{bmatrix}$$
(46)

satisfying the inequalities

$$\begin{vmatrix} \Pi_{ij} & 0 & G_i A_i + L_i C_{i2} & G_i B_{i2} + L_i D_{i21} \\ * & -I & \bar{C}_{i1} & D_{i12} \\ * & * & -\bar{P}_i & 0 \\ * & * & * & -\gamma^2 I \end{vmatrix} < 0,$$
$$\forall (i,j) \in S \ (47)$$

where  $\Pi_{ij} = \bar{P}_j - G_i - G_i^{\mathrm{T}}$  and

$$\bar{A}_{i} = T_{bi}A_{i}T_{bi}^{-1}, \quad \bar{B}_{i2} = T_{bi}B_{i2}$$
$$\bar{C}_{i1} = C_{i1}T_{bi}^{-1}, \quad \bar{C}_{i2} = C_{i2}T_{bi}^{-1}$$
(48)

and  $T_{bi}$  are given by (44), then the piecewise linear system (38) is stabilized by the SOF controller (3) and the  $H_{\infty}$ -norm of the closed-loop system (41) is smaller than  $\gamma$ , i.e.,  $\sum_{k=0}^{N} \|\boldsymbol{z}(k)\|^2 < \gamma^2 \sum_{k=0}^{N} \|\boldsymbol{w}(k)\|^2$ . The control gains  $K_i$  can be obtained by

$$K_i = G_{i11}^{-1} L_{i1}, \quad i \in I_l$$
(49)

**Proof.** Assume that LMIs (47) are feasible and define  $P_j = T_{bi}^{\mathrm{T}} \bar{P}_j T_{bi}, P_i = T_{bi}^{\mathrm{T}} \bar{P}_i T_{bi}$ . Then,

$$\bar{P}_j = T_{bi}^{-\mathrm{T}} P_j T_{bi}^{-1}, \quad \bar{P}_i = T_{bi}^{-\mathrm{T}} P_i T_{bi}^{-1}$$
 (50)

Substituting (48) and (50) into (47) leads to

$$\begin{bmatrix} \Upsilon_{ij} & 0 & G_i T_{bi} A_i T_{bi}^{-1} + L_i C_{i2} T_{bi}^{-1} & \Gamma_i \\ * & -I & C_{i1} T_{bi}^{-1} & D_{i12} \\ * & * & -T_{bi}^{-T} P_i T_{bi}^{-1} & 0 \\ * & * & * & -\gamma^2 I \end{bmatrix} < 0,$$

where  $\Upsilon_{ij} = T_{bi}^{-\mathrm{T}} P_j T_{bi}^{-1} - G_i - G_i^{\mathrm{T}}, \Gamma_i = G_i T_{bi} B_{i2} + L_i D_{i21}.$ Pre- and post-multiplying (51) by

$$\left[ \begin{array}{cccc} T_{bi}^{\mathrm{T}} & 0 & 0 & 0 \\ 0 & I & 0 & 0 \\ 0 & 0 & T_{bi}^{\mathrm{T}} & 0 \\ 0 & 0 & 0 & I \end{array} \right]$$

and its transpose yields

$$\begin{bmatrix} \Phi_{ij} & 0 & T_{bi}^{\mathrm{T}}G_{i}T_{bi}A_{i} + T_{bi}^{\mathrm{T}}L_{i}C_{i2} & \Lambda_{i} \\ * & -I & C_{i1} & D_{i12} \\ * & * & -P_{i} & 0 \\ * & * & * & -\gamma^{2}I \end{bmatrix} < 0,$$
$$\forall (i, j) \in S \ (52)$$

where

$$\Phi_{ij} = P_j - T_{bi}^{\mathrm{T}} G_i T_{bi} - T_{bi}^{\mathrm{T}} G_i^{\mathrm{T}} T_{bi}$$
$$\Lambda_i = T_{bi}^{\mathrm{T}} G_i T_{bi} B_{i2} + T_{bi}^{\mathrm{T}} L_i D_{i21}$$

From the structure of  $L_i$  and  $G_i$  and from (43) and (49), we have

$$L_{i} = \begin{bmatrix} L_{i1} \\ 0 \end{bmatrix} = \begin{bmatrix} G_{i11}K_{i} \\ 0 \end{bmatrix} = \begin{bmatrix} G_{i11} & G_{i12} \\ 0 & G_{i22} \end{bmatrix} \begin{bmatrix} I \\ 0 \end{bmatrix} K_{i} = G_{i}T_{bi}B_{i1}K_{i}$$
(53)

By simple algebraic operation, we can obtain

$$T_{bi}^{T}G_{i}T_{bi}A_{i} + T_{bi}^{T}L_{i}C_{i2} = T_{bi}^{T}G_{i}T_{bi}A_{cli}$$
$$T_{bi}^{T}G_{i}T_{bi}B_{i2} + T_{bi}^{T}L_{i}D_{i21} = T_{bi}^{T}G_{i}T_{bi}B_{cli}$$
(54)

Due to the assumption that  $D_{i11} = 0$ , we have

$$C_{i1} = C_{cli}, \quad D_{i12} = D_{cli}$$
 (55)

By substituting (54) and (55) into (52), it follows that

$$\begin{bmatrix} \Phi_{ij} & 0 & T_{bi}^{\mathrm{T}}G_{i}T_{bi}A_{cli} & T_{bi}^{\mathrm{T}}G_{i}T_{bi}B_{cli} \\ * & -I & C_{cli} & D_{cli} \\ * & * & -P_{i} & 0 \\ * & * & * & -\gamma^{2}I \end{bmatrix} < 0, \\ \forall (i,j) \in S \quad (56)$$

Inequalities (56) can be written in the form

$$P + XH + H^{\mathrm{T}}X^{\mathrm{T}} < 0, \quad \forall (i,j) \in S$$
(57)

where

$$P = \begin{bmatrix} P_j & 0 & 0 & 0\\ 0 & I & 0 & 0\\ 0 & 0 & -P_i & 0\\ 0 & 0 & 0 & -\gamma^2 I \end{bmatrix}, \quad X = \begin{bmatrix} T_{bi}^{\mathrm{T}} G_i T_{bi} & 0\\ 0 & I\\ 0 & 0\\ 0 & 0 \end{bmatrix}$$
$$H = \begin{bmatrix} -I & 0 & A_{cli} & B_{cli}\\ 0 & -I & C_{cli} & D_{cli} \end{bmatrix}$$
(58)

In addition, the closed-loop piecewise linear system (41) can be written in the form

$$H\boldsymbol{\xi}(k) = 0 \tag{59}$$

where

$$\boldsymbol{\xi}(k) = \begin{bmatrix} \boldsymbol{x}(k+1) \\ \boldsymbol{z}(k) \\ \boldsymbol{x}(k) \\ \boldsymbol{w}(k) \end{bmatrix}$$
(60)

It follows from Finsler's lemma that (57) is equivalent to

$$\boldsymbol{\xi}^{\mathrm{T}}(k) P \boldsymbol{\xi}(k) < 0 \tag{61}$$

Substituting (58) and (60) into (62) yields

$$\boldsymbol{x}^{\mathrm{T}}(k+1)P_{j}\boldsymbol{x}(k+1) - \boldsymbol{x}^{\mathrm{T}}(k)P_{i}\boldsymbol{x}(k) < \gamma^{2}\boldsymbol{w}^{\mathrm{T}}(k)\boldsymbol{w}(k) - \boldsymbol{z}^{\mathrm{T}}(k)\boldsymbol{z}(k), \quad \forall (i,j) \in S$$
(62)

It follows from (47) and (50) that

 $P_i = P_i^{\mathrm{T}} > 0$ 

Based on Lemma 4, the closed-loop piecewise linear system is exponentially stable and the  $H_{\infty}$ -norm is smaller than  $\gamma$ .

**Theorem 4.** Assume that  $D_{i21}$  are null matrices and  $C_{i2}$ ,  $i = 1, \dots, l$  are full row rank matrices. If there exist

symmetric matrices  $\bar{P}_i$  and  $\bar{P}_j \in \mathbf{R}^{n \times n}$  and matrices  $G_i \in \mathbf{R}^{n \times n}$  and  $L_i \in \mathbf{R}^{m \times n}$  with the following structure

$$G_i = \begin{bmatrix} G_{i11} & 0 \\ G_{i21} & G_{i22} \end{bmatrix}, \quad L_i = \begin{bmatrix} L_{i1} & 0 \end{bmatrix}$$
(63)

satisfying the inequalities

$$\begin{bmatrix} \bar{P}_{j} - G_{i} - G_{i}^{\mathrm{T}} & * & * & * \\ 0 & -I & * & * \\ \bar{A}_{i}G_{i} + \bar{B}_{i1}L_{i} & \bar{B}_{i2} & -\bar{P}_{i} & * \\ \bar{C}_{i1}G_{i} + D_{i11}L_{i} & D_{i12} & 0 & -\gamma^{2}I \end{bmatrix} < 0,$$

$$\forall (i,j) \in S \quad (64)$$

where

$$\bar{A}_{i} = T_{ci}^{-1} A_{i} T_{ci}, \quad \bar{B}_{i1} = T_{ci}^{-1} B_{i1}$$
$$\bar{B}_{i2} = T_{ci}^{-1} B_{i2}, \qquad \bar{C}_{i1} = C_{i1} T_{ci}$$
(65)

and  $T_{ci}$  are given in (44), then the piecewise linear system (38) is stabilized by the SOF controller (3) and the  $H_{\infty}$ -norm of the closed-loop system (41) is smaller than  $\gamma$ , i.e.,  $\sum_{k=0}^{N} \|\boldsymbol{z}(k)\|^2 < \gamma^2 \sum_{k=0}^{N} \|\boldsymbol{w}(k)\|^2$ . The control gains  $K_i$  can be obtained by

$$K_i = L_{i1} G_{i11}^{-1}, \quad i \in I_l$$
 (66)

**Proof.** Assume that the LMI conditions (64) are feasible. Define  $P_j = T_{ci}\bar{P}_jT_{ci}^{\mathrm{T}}$  and  $P_i = T_{ci}\bar{P}_iT_{ci}^{\mathrm{T}}$ . Then,

$$\bar{P}_j = T_{ci}^{-1} P_j T_{ci}^{-\mathrm{T}}, \quad \bar{P}_i = T_{ci}^{-1} P_i T_{ci}^{-\mathrm{T}}$$
 (67)

Substituting (65) and (67) into (64) yields

$$\begin{bmatrix} T_{ci}^{-1}P_jT_{ci}^{-T} - G_i - G_i^{T} & * & * & * \\ 0 & -I & * & * \\ T_{ci}^{-1}A_iT_{ci}G_i + T_{ci}^{-1}B_{i1}L_i & T_{ci}^{-1}B_{i2} & \Omega_i & * \\ C_{i1}T_{ci}G_i + D_{i11}L_i & D_{i12} & 0 & -\gamma^2 I \end{bmatrix} < 0,$$

$$\forall (i,j) \in S$$
(68)

where  $\Omega_i = -T_{ci}^{-1} P_i T_{ci}^{-T}$ . Pre- and post-multiplying (68) by

$$\left[ \begin{array}{cccc} T_{ci} & 0 & 0 & 0 \\ 0 & I & 0 & 0 \\ 0 & 0 & T_{ci} & 0 \\ 0 & 0 & 0 & I \end{array} \right]$$

and its transpose leads to

$$\begin{bmatrix} P_{j} - T_{ci}G_{i}T_{ci}^{\mathrm{T}} - T_{ci}G_{i}^{\mathrm{T}}T_{ci}^{\mathrm{T}} & * & * & * \\ 0 & -I & * & * \\ A_{i}T_{ci}G_{i}T_{ci}^{\mathrm{T}} + B_{i1}L_{i}T_{ci}^{\mathrm{T}} & B_{i2} & -P_{i} & * \\ C_{i1}T_{ci}G_{i} + D_{i11}L_{i} & D_{i12} & 0 & -\gamma^{2}I \end{bmatrix} < 0,$$

$$\forall (i, j) \in S$$
(69)

From the structure of  $L_i$  and  $G_i$ , and from (43) and (66), we have

$$L_{i} = \begin{bmatrix} L_{i1} & 0 \end{bmatrix} = \begin{bmatrix} K_{i}G_{i11} & 0 \end{bmatrix} = K_{i}\begin{bmatrix} I & 0 \end{bmatrix} \begin{bmatrix} G_{i11} & 0 \\ G_{i21} & G_{i22} \end{bmatrix} = K_{i}C_{i2}T_{ci}G_{i}$$
(70)

$$A_i T_{ci} G_i T_{ci}^{\mathrm{T}} + B_{i1} L_i T_{ci}^{\mathrm{T}} = A_{cli} T_{ci} G_i T_{ci}^{\mathrm{T}}$$
$$C_{i1} T_{ci} G_i + D_{i11} L_i = C_{cli} T_{ci} G_i$$
(71)

Due to the assumption that  $D_{i21} = 0$ , we have

$$B_{i2} = B_{cli}, \quad D_{i12} = D_{cli}$$
 (72)

By substituting (71) and (72) into (69), it follows that

$$\begin{bmatrix} P_{j} - T_{ci}G_{i}T_{ci}^{\mathrm{T}} - T_{ci}G_{i}^{\mathrm{T}}T_{ci}^{\mathrm{T}} & * & * & * \\ 0 & -I & * & * \\ A_{cli}T_{ci}G_{i}T_{ci}^{\mathrm{T}} & B_{cli} & -P_{i} & * \\ C_{cli}T_{ci}G_{i} & D_{cli} & 0 & -\gamma^{2}I \end{bmatrix} < 0,$$

$$\forall (i,j) \in S$$
(73)

Inequalities (73) can be rewritten in the form

$$P + XH + H^{\mathrm{T}}X^{\mathrm{T}} < 0, \quad \forall (i,j) \in S$$
(74)

where

$$P = \begin{bmatrix} P_j & 0 & 0 & 0\\ 0 & I & 0 & 0\\ 0 & 0 & -P_i & 0\\ 0 & 0 & 0 & -\gamma^2 I \end{bmatrix}$$
(75)

$$X = \begin{bmatrix} T_{ci}G_{i}T_{ci}^{\mathrm{T}} & 0\\ 0 & I\\ 0 & 0\\ 0 & 0 \end{bmatrix}, \quad H = \begin{bmatrix} -I & 0 & A_{cli}^{\mathrm{T}} & C_{cli}^{\mathrm{T}}\\ 0 & -I & B_{cli}^{\mathrm{T}} & D_{cli}^{\mathrm{T}} \end{bmatrix}$$
(76)

Consider the dual system of (41)

$$\boldsymbol{x}'(k+1) = A_{cli}^{\mathrm{T}}\boldsymbol{x}'(k) + C_{cli}^{\mathrm{T}}\boldsymbol{w}'(k)$$
$$\boldsymbol{z}'(k) = B_{cli}^{\mathrm{T}}\boldsymbol{x}'(k) + D_{cli}^{\mathrm{T}}\boldsymbol{w}'(k)$$
(77)

0

which can be written in the form

$$H\boldsymbol{\xi}'(k) =$$

where

$$\boldsymbol{\xi}'(k) = \begin{bmatrix} \boldsymbol{x}'(k+1) \\ \boldsymbol{z}'(k) \\ \boldsymbol{x}'(k) \\ \boldsymbol{w}'(k) \end{bmatrix}$$
(78)

It follows from Finsler's lemma that (74) is equivalent to

$$\boldsymbol{\xi}^{\prime \mathrm{T}}(k) P \boldsymbol{\xi}^{\prime}(k) < 0 \tag{79}$$

Substituting (76) and (78) into (79) yields

$$\boldsymbol{x}^{'^{\mathrm{T}}}(k+1)P_{j}\boldsymbol{x}^{'}(k+1) - \boldsymbol{x}^{'^{\mathrm{T}}}(k)P_{i}\boldsymbol{x}^{'}(k) < \gamma^{2}\boldsymbol{w}^{'^{\mathrm{T}}}(k)\boldsymbol{w}^{'}(k) - \boldsymbol{z}^{'^{\mathrm{T}}}(k)\boldsymbol{z}^{'}(k), \quad \forall (i,j) \in S$$
(80)

It follows from (64) and (67) that

$$P_i = P_i^{\mathrm{T}} > 0$$

Based on Lemma 4, the closed-loop piecewise linear system is exponentially stable and the  $H_{\infty}$ -norm is smaller than  $\gamma$ .

**Remark 4.** Theorems 3 and 4 present sufficient LMI conditions for  $H_{\infty}$  SOF control for discrete-time piecewise

linear systems. By using Finsler's lemma, a set of slack variables  $G_i$  with special structure are introduced to improve  $H_{\infty}$  performance and to reduce design conservatism. Note that by letting  $C_i = I$  in (4) or  $C_{i2} = I$  in (38) and slack variables  $G_i$  be general matrices, SOF control in Theorems  $1 \sim 4$  reduces to the state-feedback control in [14].

**Remark 5.** In Theorems 1 and 2, it is assumed that  $B_i$  are of full column rank or  $C_i$  are of full row rank. If this assumption is not satisfied, i.e., both  $B_i$  and  $C_i$  are not of full rank, we can introduce non-singular linear transformation to system (1) and obtain a new system model satisfying the assumption<sup>[27]</sup>. Then, Theorems 1 and 2 can be used for the newly-built model. Therefore, this method can also be used to deal with the situation where both  $B_{i1}$  and  $C_{i2}$  in system (38) are not of full rank.

### 4 Examples

In this section, three examples are given to illustrate the effectiveness of our method. Examples 1 and 2 provide a comparison of the proposed method to the methods presented in [22–23]. These two examples show that our synthesis method can work successfully in situations where [22–23] do not, respectively. In Example 3, an  $H_{\infty}$  SOF controller is designed to show the effectiveness of Theorems 3 and 4.

**Example 1.** Consider the following system borrowed from [23]

$$\boldsymbol{x}(k+1) = A_i \boldsymbol{x}(k) + B_i \boldsymbol{u}(k), \quad i = 1, 2, 3, 4$$

where

$$A_{1} = \begin{bmatrix} 0.7786 & 0.9908 & 0.1270 \\ 0.1616 & 0.8443 & 0.8144 \\ 0.9214 & 0.9747 & 0.7825 \end{bmatrix}$$
$$A_{2} = \begin{bmatrix} 0.3894 & 0.3263 & 0.7746 \\ 0.7806 & 0.9886 & 0.1297 \\ 0.8814 & 0.4718 & 0.3110 \end{bmatrix}$$
$$A_{3} = \begin{bmatrix} 0.3049 & 0.4247 & 0.8979 \\ 0.8448 & 0.2485 & 0.6921 \\ 0.7558 & 0.9160 & 0.3636 \end{bmatrix}$$
$$A_{4} = \begin{bmatrix} 0.1194 & 0.3964 & 0.2454 \\ 0.1034 & 0.2515 & 0.4983 \\ 0.6981 & 0.8655 & 0.2403 \end{bmatrix}$$

and

$$B_{1} = \begin{bmatrix} 0.2458 & 0.7409\\ 0.2501 & 0.5257\\ 0 & 0 \end{bmatrix}, B_{2} = \begin{bmatrix} 0.2722 & 0.6055\\ 0.1576 & 0.1580\\ 0 & 0 \end{bmatrix}$$
$$B_{3} = \begin{bmatrix} 0.4945 & 0.3020\\ 0.9237 & 0.9118\\ 0 & 0 \end{bmatrix}, B_{4} = \begin{bmatrix} 0.9894 & 0.7205\\ 0.1709 & 0.1519\\ 0 & 0 \end{bmatrix}$$

Note that  $A_1 \sim A_4$  are all unstable. The system is allowed to switch arbitrarily between these four modes. Output matrices are selected as<sup>[23]</sup>

$C_1 = [0.3815]$	0.6916	0.7183]
$C_2 = \begin{bmatrix} 0.0591 \end{bmatrix}$	0.8258	0.4354 ]
$C_3 = [ 0.5204$	0.8010	0.9708 ]
$C_4 = \begin{bmatrix} 0.6995 \end{bmatrix}$	0.3081	0.8767

Reference [23] has shown that this system cannot be stabilized using the method in [22]. However, it can be stabilized using our method and the control gains are given as

$$K_{1} = \begin{bmatrix} -5.1512\\ 0.6370 \end{bmatrix}, \quad K_{2} = \begin{bmatrix} -4.1075\\ -0.0307 \end{bmatrix}$$
$$K_{3} = \begin{bmatrix} -3.2011\\ 2.4172 \end{bmatrix}, \quad K_{4} = \begin{bmatrix} 1.7127\\ -2.9989 \end{bmatrix}$$

These SOF control gains give the following closed-loop poles for each modes:

 $\begin{array}{l} \mbox{Mode 1: } \{0.6351, 0.4040 \pm 0.5478i\} \\ \mbox{Mode 2: } \{0.7029, 0.1902 \pm 0.6019i\} \\ \mbox{Mode 3: } \{0.4600, -0.2949 \pm 0.3924i\} \\ \mbox{Mode 4: } \{0.7737, -0.2693 \pm 0.3320i\} \end{array}$ 

**Example 2.** Consider system (1) with three modes, which is described by the following matrices:

$$A_{1} = \begin{bmatrix} 3 & 0.3 & 2 \\ 1 & 0 & 1 \\ 0.3 & 0.6 & 0.6 \end{bmatrix}$$

$$A_{2} = \begin{bmatrix} -0.5871 & -0.8441 & -0.0092 \\ -0.6865 & -0.5090 & -0.8561 \\ 0.0974 & 0.4523 & -0.2280 \end{bmatrix}$$

$$A_{3} = \begin{bmatrix} 0.1089 & 0.2458 & -0.9035 \\ 0.3998 & -0.9213 & -0.4161 \\ 0.6745 & -0.5750 & 0.7138 \end{bmatrix}$$

$$B_{1} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ 1 & 0 \end{bmatrix}, \quad B_{2} = \begin{bmatrix} 0.1930 & -0.4204 \\ -0.7359 & 0.0346 \\ 0.5073 & -0.9077 \end{bmatrix}$$

$$B_{3} = \begin{bmatrix} -0.4164 & 0.0244 \\ 0.8297 & -0.4366 \\ -0.0900 & -0.8416 \end{bmatrix}$$

Note that all the modes are unstable. The output matrices are given as

$$C_1 = \begin{bmatrix} 1 & 1 & 0 \end{bmatrix}, \quad C_2 = \begin{bmatrix} 1 & 0 & 1 \end{bmatrix}, \quad C_3 = \begin{bmatrix} 0 & 1 & 1 \end{bmatrix}$$

For this system, the method developed in [23] does not allow to compute an SOF controller. However, our method provides the following control gains:

$$K_1 = \begin{bmatrix} -0.9273\\ 0.0032 \end{bmatrix}, \quad K_2 = \begin{bmatrix} -1.0162\\ -0.4316 \end{bmatrix}, \quad K_3 = \begin{bmatrix} 0.3791\\ 0.5438 \end{bmatrix}$$

These SOF control gains give the following closed-loop poles for each modes:

$$\begin{array}{l} \text{Mode 1}: \{0.0412, 0.7174 \pm 0.6314i\} \\ \text{Mode 2}: \{0.5364, -0.4631 \pm 0.2830i\} \\ \text{Mode 3}: \{-0.8203, 0.1535 \pm 0.5217i\} \end{array}$$

**Example 3.** Consider system (38) with two modes. System matrices are given as

$A_1 =$	$\begin{bmatrix} -0.5871 \\ -0.6865 \\ 0.0974 \end{bmatrix}$	-0.8441 -0.5090 0.4523	$ \begin{array}{c} -0.0092 \\ -0.8561 \\ -0.2280 \end{array} $
$A_2 =$	$\begin{bmatrix} 0.1089 \\ 0.3998 \\ 0.6745 \end{bmatrix}$	$\begin{array}{c} 0.2458 \\ -0.9213 \\ -0.5750 \end{array}$	$\begin{bmatrix} -0.9035 \\ -0.4161 \\ 0.7138 \end{bmatrix}$

$$B_{11} = \begin{bmatrix} 0.1930 & -0.4204 \\ -0.7359 & 0.0346 \\ 0.5073 & -0.9077 \end{bmatrix}$$
$$B_{21} = \begin{bmatrix} -0.4164 & 0.0244 \\ 0.8297 & -0.4366 \\ -0.0900 & -0.8416 \end{bmatrix}$$
$$B_{12} = B_{22} = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}, \quad C_{11} = C_{21} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$
$$C_{12} = \begin{bmatrix} 1 & 0 & 1 \end{bmatrix}, \quad C_{22} = \begin{bmatrix} 0 & 1 & 1 \end{bmatrix}$$
$$D_{111} = D_{211} = \begin{bmatrix} 0 & 0 \\ 0 & 1 \\ 0 & 1 \end{bmatrix}, \quad D_{112} = \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix}, \quad D_{212} = \begin{bmatrix} 1 \\ 0 \\ 1 \end{bmatrix}$$

 $D_{121}, D_{221}$  are null matrices.

By Theorem 4, the control gains are obtained as

$$K_1 = \begin{bmatrix} -1.0832 \\ -0.5259 \end{bmatrix}, \quad K_2 = \begin{bmatrix} 0.3563 \\ -0.1241 \end{bmatrix}$$

and the  $H_{\infty}$ -norm is 5.6853.

The following two figures are the responses of openloop and closed-loop states with initial states chosen as  $\boldsymbol{x}(0) = \begin{bmatrix} -2 & 2 & 4 \end{bmatrix}^{\mathrm{T}}$  and disturbances chosen as  $w = \begin{cases} 2, & k < 10 \\ 0, & k \geq 10 \end{cases}$ . Fig. 1 shows that the open-loop system is unstable and Fig. 2 shows that the closed-loop system is exponentially stable.

### 5 Conclusion

In this paper, the problem of SOF control for discretetime piecewise linear systems has been addressed. By the aid of piecewise quadratic Lyapunov functions combined with Finsler's lemma, new sufficient LMI conditions for the synthesis of SOF stabilization controllers have been given. The proposed method can work successfully where the existing ones do not. Extension to  $H_{\infty}$  control has also been presented. The numerical examples have shown the effectiveness of the proposed methods.

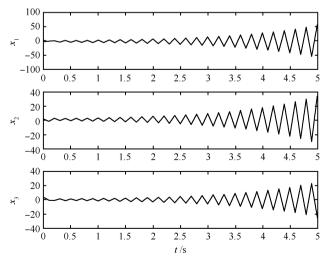


Fig. 1 Responses of open-loop states

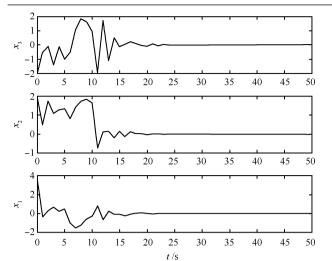


Fig. 2 Responses of closed-loop states

#### References

- 1 Xu J, Xie L. Null controllability of discrete-time planar bimodal piecewise linear systems. International Journal of Control, 2005, 78(18): 1486-1496
- 2 Bemporad A, Morari M. Control of systems integrating logic, dynamics, and constraints. Automatica, 1999, 35(3): 407-427
- 3 Schutter B D, Moor B D. The extended linear complementarity problem and the modeling and analysis hybrid systems. *Lecture Notes in Computer Science*, 1999, **1567**: 635–636
- 4 Sontag E D. Nonlinear regulation: the piecewise linear approach. IEEE Transactions on Automatic Control, 1981, 26(2): 346-358
- 5 Hassibi A, Boyd S. Quadratic stabilization and control of piecewise-linear systems. In: Proceedings of the American Control Conference. Philadephia, USA: IEEE, 1998. 3659-3664
- 6 Johansson M, Rantzer A. Computation of piecewise quadratic Lyapunov functions of hybrid systems. *IEEE Transactions on Automatic Control*, 1998, **43**(4): 555–559
- 7 Rantzer A, Johansson M. Piecewise linear quadratic optimal control. *IEEE Transactions on Automatic Control*, 2000, 45(4): 629-637
- 8 Rodrigues L, How J P. Observer-based control of piecewiseaffine systems. International Journal of Control, 2003, 76(5): 459–477
- 9 Rodrigues L, Boyd S. Piecewise-affine state feedback for piecewise-affine slab systems using convex optimization. Systems Control Letters, 2005, 54(9): 835-853
- 10 Chen M, Zhu C R, Feng G. Linear-matrix-inequality-based approach to  $H_{\infty}$  controller synthesis of uncertain continuoustime piecewise linear systems. *IEE Proceedings* — *Control Theory and Applications*, 2004, **151**(3): 295–301
- 11 Zhu Y, Li D Q, Feng G.  $H_{\infty}$  controller synthesis of uncertain piecewise continuous-time linear systems. *IEE Proceedings* — Control Theory and Applications, 2005, **152**(5): 513–519
- 12 Mignone D, Ferrari-Trecate G, Morari M. Stability and stabilization of piecewise affine and hybrid systems: an LMI approach. In: Proceedings of the 39th IEEE Conference on Decision and Control. Sydney, Australia: IEEE, 2000. 504–509
- 13 Ferrari-Trecate G, Cuzzola F A, Mignone D, Morari M. Analysis and control with performance of piecewise affine and hybrid systems. In: Proceedings of the American Control Conference. Arlington, USA: IEEE, 2001. 200–205
- 14 Ferrari-Trecate G, Cuzzola F A, Mignone D, Morari M. Analysis of discrete-time piecewise affine and hybrid systems. Automatica, 2002, 38(12): 2139–2146

- 15 Cuzzola F A, Morari M. An LMI approach for  $H_{\infty}$  analysis and control of discrete-time piecewise affine systems. International Journal of Control, 2002, **75**(16-17): 1293–1301
- 16 Feng G. Stability analysis of piecewise discret-time linear systems. *IEEE Transactions on Automatic Control*, 2002, 47(7): 1108–1112
- 17 Feng G. Observer-based output feedback controller design of piecewise discrete-time linear systems. *IEEE Transactions on Circuits and Systems I: Fundamental Theory and Application*, 2003, **50**(3): 448–451
- 18 Syrmos V L, Abdallah C T, Dorato P, Grigoriadis K. Static output feedback — a survey. Automatica, 1997, 33(2): 125–137
- 19 Lee K H, Lee J H, Kwon W H. Sufficient LMI conditions for  $H_{\infty}$  output feedback stabilization of linear discrete-time systems. *IEEE Transactions on Automatic Control*, 2006, **51**(4): 675–680
- 20 Dong J X, Yang G H. Static output feedback control synthesis for linear systems with time-invariant parametric uncertainties. *IEEE Transactions on Automatic Control*, 2007, 52(10): 1930–1936
- 21 Dong J X, Yang G H. Robust static output feedback control for linear discrete-time systems with time-varying uncertainties. Systems and Control Letters, 2008, 57(2): 123–131
- 22 Daafouz J, Riedinger P, Iung C. Stability analysis and control synthesis for switched systems: a switched Lyapunov function approach. *IEEE Transactions on Automatic Control*, 2002, **47**(11): 1883–1887
- 23 Bara G M, Boutyeb M. Switched output feedback stabilization of discrete-time switched systems. In: Proceedings of the 45th IEEE Conference on Decision and Control. San Diego, USA: IEEE, 2006. 2667–2672
- 24 de Oliveira M C, Bernussou J, Geromel J C. A new discretetime robust stability condition. Systems and Control Letters, 1999, 37(4): 261–265
- 25 Boyd S, Ghaoui L E, Feron E, Balakrishnan V. Linear Matrix Inequalities in Systems and Control Theory. Philadelphia: Society for Industrial Mathematics, 1994
- 26 Gahinet P, Nemirovski A, Laub A, Chilali M. The LMI Control Toolbox. Natick: Mathworks, 1995
- 27 Kailath T. Linear Systems. Englewood Cliffs: Prentice-Hall, 1980



**DING Da-Wei** Ph. D. candidate at the College of Information Science and Engineering, Northeastern University. His research interest covers switched systems, fault-tolerant control, and robust control. Corresponding author of this paper. E-mail: ddaweiauto@163.com



YANG Guang-Hong Professor at the College of Information Science and Engineering, Northeastern University. His research interest covers fault-tolerant control, fault detection and isolation, and robust control.

E-mail: yangguanghong@ise.neu.edu.cn